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Rotational Diffusion Coefficient (or Rotational Mobility) of a Nanorod in the Free-Molecular Regime

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The corrected rotational diffusion coefficient for a rod in the free molecular regime is given in this work and a simplified derivation using the differential drag forces for a rotating rod in the free molecular regime is presented to explain the difference between our result and the one from Kim's approach. Finally, we compare the rotational diffusion coefficient between a rod and an ellipsoid with the same aspect ratio and the same volume.

1. INTRODUCTION

Rotational diffusion coefficient, which is related to rotational mobility, is the characteristic value of the Brownian rotation of a particle. This quantity is important in studies of the alignment of nonspherical particles in an electric field (Li 2012; Li et al. 2012, 2013a,b). The theory for rotational Brownian diffusion coefficient of dilute suspensions of axially symmetric particles in the continuum regime has been studied by a number of researchers (Brenner 1974; Brenner and Condiff 1974; Ortega and de la Torre 2003). In the free molecular regime, Halbritter (1974) calculated the rotational torque for a general convex-shaped particle and obtained an explicit torque expression for an ellipsoid (Halbritter 1974; Williams and Loyalka 1991). Eisner and Gallily (1981) calculated the rotational diffusion coefficient of nonspherical aerosol particles and obtained an explicit rotational diffusion coefficient expression for a rod. However, Eisner and Gallily (1981) did not express the moment of specular reflection correctly. In Equation (3.6) of Eisner and Gallily (1981), the velocities should be relative to the particle surface, i.e., (v_1, v_1') , instead of to the observer, (v_2, v_2')). The corrected rotational diffusion coefficient for a rod in the free molecular regime, using a common definition of rod aspect ratio $\beta = L_r/d_r$, is

$$D_{\rm r,f} = \frac{k_{\rm B}TK_n}{\pi\mu L_r^3 \left[\left(\frac{1}{6} + \frac{1}{8\beta^3}\right) + f\left(\frac{\pi-2}{48} + \frac{1}{8\beta} + \frac{1}{8\beta^2} + \frac{\pi-4}{8}\frac{1}{8\beta^3}\right) \right]},$$
[1]

where k_B is the Boltzmann constant, T is the absolute temperature, the Knudsen number $K_n = 2\lambda/d_r$, λ is the mean free path of gas, d_r is the rod diameter, L_r is the rod length, μ is the gas viscosity, and f is the momentum accommodation. To compare with our result, we give Eisner and Gallily's uncorrected equation (Eisner and Gallily 1981):

$$D_{\rm r,f} = \frac{k_{\rm B}TK_{\rm n}}{\pi\,\mu L_r^3 \Big[\Big(\frac{1}{4} + \frac{1}{4\beta} + \frac{1}{4\beta^2} + \frac{1}{8\beta^3}\Big) + f\Big(\frac{\pi-6}{48} - \frac{1}{8\beta} - \frac{1}{8\beta^2} + \frac{\pi-4}{8}\frac{1}{8\beta^3}\Big) \Big]}.$$
[2]

The difference between the two expressions is 5-10% for a momentum accommodation, f, of 0.9 and rod aspect ratio β greater than 2.

2. DERIVATIONS AND DISCUSSIONS

The corrected rotational diffusion coefficient for a rod in the free molecular regime, i.e., Equation (1), can be obtained by repeating the derivation procedures in Eisner and Gallily (1981) but using the correct velocity relationship for specular reflection as mentioned earlier. In this work, we show another derivation for Equation (1) using the differential drag forces for a rotating rod in the free molecular regime and explain the difference



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FIG. 1. A rotational rod (with angular velocity $\omega \vec{i}$) in a coordinate system $(\vec{i}, \vec{j}, \vec{k})$.

between our result and the one from Kim's approach (Kim et al. 2007).

Halbritter (1974) calculated the differential drag forces for a general convex particle with an angular velocity ω in the free molecular regime (Halbritter 1974, Equation 8). We apply the general equation to calculate the differential drag forces for a rotational rod with an angular velocity ω (Figure 1). Assuming that the rod (with length L_r and diameter $d_r = 2\rho$) rotates along the \vec{i} axis, for a small patch on the curved portion of the cylindrical surface with coordinates ($\rho \cos \phi$, $\rho \sin \phi$, z), the differential forces along the \vec{j} axis, dF_j^c , and along the \vec{k} axis, dF_k^c , are

$$dF_{j}^{c} = \frac{\mu}{\lambda}\omega z \left[\left(2 - \frac{4-\pi}{4}f \right) \sin^{2}\phi + \frac{1}{2}f \cos^{2}\phi \right] dS^{c}, \quad [3]$$

$$dF_k^c = -\frac{\mu}{2\lambda} f \,\omega\rho \sin\phi dS^c, \qquad [4]$$

where $dS^c = \rho d\phi dz$ and the integration range $-\frac{L_r}{2} \le z \le \frac{L_r}{2}$, $0 \le \phi \le 2\pi$.

For a small patch on the flat-end surface with coordinates $(\rho' \cos\phi, \rho' \sin\phi, L_r/2)$, the differential forces along the \vec{j} axis, dF_j^{e} , and along the \vec{k} axis, dF_k^{e} , are

$$dF_{j}^{e} = \frac{\mu}{2\lambda} f \omega \frac{L_{r}}{2} dS^{e}, \qquad [5]$$

$$dF_k^e = -\left(2 - \frac{4 - \pi}{4}f\right)\frac{\mu}{\lambda}\omega\rho'\sin\phi dS^e,\qquad[6]$$

where $dS^e = \rho' d\phi d\rho'$ and the integration range $0 \le \rho' \le \rho$, $0 \le \phi < 2\pi$.

Then, the total torque, M, along the \vec{i} axis can be obtained by considering the contribution from forces along \vec{j} axis and \vec{k} axis for the curved cylindrical surface (1st integral) and the two flat-end surfaces (2nd integral) as

$$M = \int \left(-zdF_{j}^{c} + \rho \sin\phi dF_{k}^{c} \right) + 2 \int \left(-\frac{L}{2}dF_{j}^{e} + \rho' \sin\phi dF_{k}^{e} \right)$$
$$= \pi \mu L_{r}^{3} \left[\left(\frac{1}{6} + \frac{1}{8\beta^{3}} \right) + f \left(\frac{\pi - 2}{48} + \frac{1}{8\beta} + \frac{1}{8\beta^{2}} + \frac{\pi - 4}{8\beta^{3}} \frac{1}{8\beta^{3}} \right) \right] \frac{d_{r}\omega}{2\lambda}.$$
[7]

Then, the rotational mobility is $B_{\omega} = \omega/M$, and the rotational diffusion coefficient is $D_{r,f} = k_B T B_{\omega}$, which gives Equation (1).

The differential forces parallel to the velocity direction, i.e., dF_j^c in Equation (3) and dF_j^e in Equation (5), are identical to the differential forces in Equation (21) of Dahneke (1973) on substituting drifting velocity $V_d = -\omega z$ and $V_d = -\omega L_r/2$, respectively. However, the differential forces perpendicular to the velocity direction for a rotational movement (dF_k^c in Equation (4) and dF_k^e in Equation (6), respectively) are different from the forces for a constant translational movement which are zero as given by Dahneke (1973).

2.1. Comparing our Result in Equation (1) with Kim's Approach

In the free molecular regime, Kim et al. (2007) used a much simpler but approximate method to obtain the rotational diffusion coefficient of a rod by applying the drag forces from Dahneke (1973). Since Dahneke's drag force expressions were presented for a rod with a constant translational movement as we discussed earlier, Kim's approach calculated the torque from the forces parallel to the velocity direction, but did not consider the torque from the forces perpendicular to the velocity direction. Even though the sum of the forces perpendicular to the velocity direction is zero, the sum of the torque from those forces is not zero. However, if the rod diameter is much smaller than the length, i.e., for $1/\beta$ small, the torque from the forces perpendicular to the velocity direction can be neglected, which makes Kim's approach a good approximation for a slender rod. After correcting the missing factor of "2" (Kim et al. considered the rotational resistance of only half of the rod), and considering the effect of the two ends of the rod using Kim's approach, we obtain

$$D_{\rm r,f} = \frac{k_{\rm B}TK_{\rm n}}{\pi\mu L_r^3 \left[\frac{1}{6} + f\left(\frac{\pi-2}{48} + \frac{1}{8\beta}\right)\right]}.$$
 [8]

To order $1/\beta$, Equations (8) and (1) are identical.

2.2. Comparing the Rotational Diffusion Coefficient Between a Rod in Equation (1) and an Ellipsoid

We make use of the explicit expression for the torque of an ellipsoid (Equation 13 of Halbritter, 1974) to compute its rotational diffusion coefficient, and compare it with Equation (1). The ratio between the rotational diffusion coefficient of an



FIG. 2. Rotational diffusion coefficient ratio between an ellipsoid and a rod with the same volume and the same aspect ratio for a rod diameter $d_r = 15$ nm.

ellipsoid and a rod with the same volume and the same aspect ratio is plotted in Figure 2 assuming a rod diameter $d_r = 15$ nm and a momentum accommodation f = 0.9. The difference in the rotational diffusion coefficients for a rod and an ellipsoid with the same aspect ratio and same volume is less than 2.2% for aspect ratios larger than 20.

3. CONCLUSIONS

The corrected rotational diffusion coefficient for a rod in the free molecular regime is given in this work and a simplified derivation using the differential drag forces for a rotating rod in the free molecular regime is presented to explain the difference between our result and the one from Kim's approach (Kim et al. 2007). Finally, we compare the rotational diffusion coefficient between a rod and an ellipsoid with the same aspect ratio and the same volume.

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